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Monthly Performance Report

REEDY CREEK UTILITIES

JUNE 1979



U.S. Department of Energy

National Solar Heating and Cooling Demonstration Program

National Solar Data Program

_ NOTICE _

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MONTHLY PERFORMANCE REPORT REEDY CREEK UTILITIES JUNE 1979

SYSTEM DESCRIPTION

The Reedy Creek site is a two story, 6,100 square foot concrete block office building located in Lake Buena Vista, Florida. The solar energy system is designed to provide space heating, domestic hot water and space cooling.

The collector subsystem is composed of a horizontal array of 16 parabolic trough collectors, manufactured by AAI Corporation, with tracking absorber tubes. The collector array is an integral part of the building's roof, with the reflector troughs oriented so that each major axis is in an east-west direction. The 16 absorber tubes are moved in unison in a north-south direction by the solar tracking system. The total collector aperture area is 3,840 square feet. Water is used as the heat collection, transfer, and storage medium. Collected solar energy is stored in a 10,000-gallon hot water tank, located adjacent to the building and shaded by the roof. Domestic hot water is provided by a heat exchanger immersed in this tank. Space heating is provided by circulation of hot water from the storage tank through heat exchangers located in the central air distribution system. No auxiliary energy is provided for either domestic hot water or space heating.

A 25-ton absorption chiller utilizes hot water from solar storage to provide chilled water to a 10,000-gallon cold water storage tank. For space cooling, water from this cold tank is circulated through heat exchangers located in the building's central air distribution system. Auxiliary cooling is provided by supplemental cold water from the utility district's central chiller plant, which is powered by fossil fuels.

The system, shown schematically in Figure 1, has five modes of solar operation.

Mode 1 - Collector-to-Storage: This mode is entered when the collector absorber plate temperature is 10°F higher than the temperature at the bottom of the hot storage tank (water solar thermal storage). Water is circulated through the collector array-storage loop by pump Pl until the temperature of the water at the bottom of storage rises to within 3°F of that of the collector absorber plate.

Mode 2 - Storage-to-Space Heating: This mode is entered when the temperature falls below the setting of the thermostats located in the occupied areas. Since this is the only means of space heating available, no minimum tank temperature is specified. Pump P2 causes hot water to flow directly from the storage tank to the heat exchanger in the air-handling unit, and back to the storage tank.

Mode 3 - Domestic Hot Water Heating: Domestic hot water (DHW) is provided by passing city supply water through a heat exchanger immersed in the solar thermal storage tank. No conventional water heater exists, thus water is heated only upon demand. A tempering valve is used when necessary to reduce the temperature of water leaving the heat exchanger. If the water is too hot, cold supply water is mixed with it in the tempering valve before going to the DHW line.

Mode 4 - Chilled Water Production: This mode is entered when the temperature of the water in the top of the solar thermal storage tank is at or above the generator operating temperature (nominally 180°F) and that of the water at the bottom of the 10,000-gallon chilled water storage is greater than 45°F. Hot water is drawn from the solar thermal storage tank to operate the generator section of the absorption chiller and cold water is circulated through the chiller from the chilled water storage. Energy is removed from the cold water, lowering its temperature; the energy is rejected through the cooling tower, and the cold water returns to the chilled water storage tank. Whenever the temperature

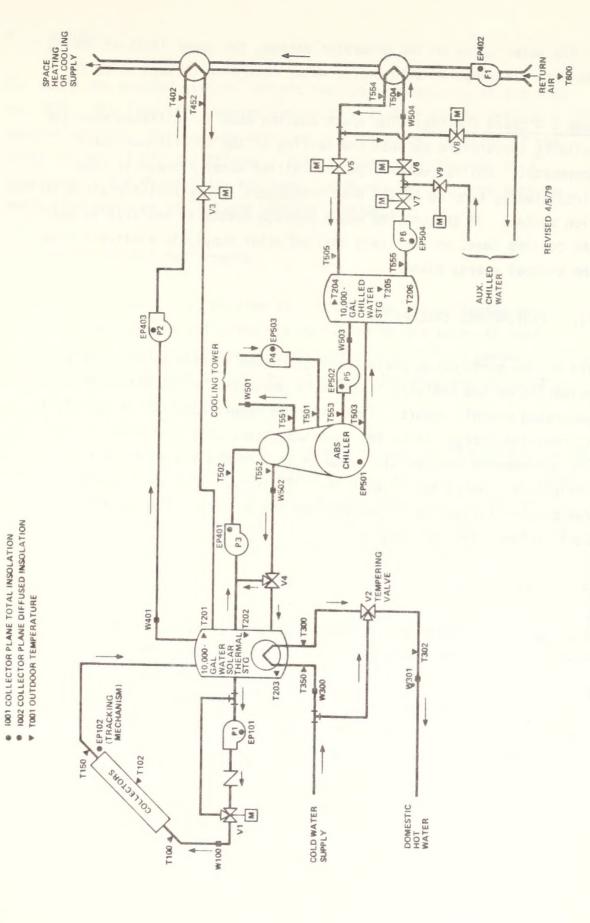


Figure 1. REEDY CREEK SOLAR ENERGY SYSTEM SCHEMATIC

of the water going to the generator exceeds the upper limit of 195°F, the water is tempered with cooler water returning through valve V4.

Mode 5 - Space Cooling: The space cooling mode is initiated when the building temperature exceeds the setting of the conditioned space thermostat. Chilled water from the chilled water storage is then circulated by pump P6 to the heat exchangers in the building air distribution system. If the chilled water storage system is not able to meet the cooling load, an auxiliary chilled water supply is available from the central energy plant.

II. PERFORMANCE EVALUATION

The system performance evaluations discussed in this section are based primarily on the analysis of the data presented in the attached computer-generated monthly report. This attached report consists of daily site thermal and energy values for each subsystem, plus environmental data. The performance factors discussed in this report are based upon the definitions contained in NBSIR 76-1137, Thermal Data Requirements and Performance Evaluation Procedures for the National Solar Heating and Cooling Demonstration Program.

A. Introduction

The Reedy Creek solar energy system operated continuously throughout the month of June. The DHW demand was 0.16 million Btu, there was no space heating demand, and the space cooling demand was 18.78 million Btu. The solar energy system supplied 100 percent of the DHW requirement, and 43 percent of the space cooling requirements - these quantities are reported in the attached computer printout as loads.

B. Weather

For June, the average outside ambient temperature measured at the site was 82°F. The long-term average temperature is 81°F at the Orlando weather station. The average measured insolation in the plane of the array was only 1,826 Btu/ft^2 -day. This is very near the long-term average of 1,830 Btu/ft^2 -day for June, which was derived from measurements also taken at the Orlando weather station.

C. System Thermal Performance

<u>Collector</u> - Of the 210.33 million Btu incident on the collector array, 21.17 million Btu were collected and delivered to the solar thermal storage tank. This represents an array efficiency of 10.1 percent. Operating energy of 1.19 million Btu (348 kwh) was required to collect and store this solar energy.

<u>Storage</u> - Of the 21.17 million Btu delivered to storage, 13.59 million Btu were subsequently removed for use within the system. Temperature probes within the solar thermal storage tank indicate that the internal energy of the water increased by 0.43 million Btu during the month. This indicates a resulting loss to the environment of 7.15 million Btu through the tank insulation.

<u>Domestic Hot Water</u> - DHW is provided to the building by passing city water through a heat exchanger that is immersed in the solar thermal storage tank. A total of 303 gallons of water at an average temperature of 134°F was supplied by the system during June. The average temperature increase was 64°F, which resulted in a measured demand of 0.16 million Btu. All of this energy was supplied by the solar energy system. There was no operating energy required.

Space Heating - No space heating was required during the month of June.

Absorption Chiller - The absorption chiller operated on 11 occasions to reduce the chilled water storage temperature during June. A total of 4.29 million Btu of electrical energy from the auxiliary conventional cooling system was required to assist the absorption chiller to meet the cooling load on 23 days of the month. The absorption chiller utilized 13.43 million Btu from the solar thermal storage tank to remove 7.36 million Btu from the chilled water storage (see attached Auxiliary Performance data). The resulting coefficient of performance (COP) of 0.548 is very near the average of the past 10 months.

Chilled Water Storage - Performance of the chilled water storage (see attached Auxiliary Storage Performance data) shows that 7.36 million Btu were removed by the chiller, 8.06 million Btu were added from the conditioned space during cooling, and the internal energy of the chilled water storage increased by 0.31 million Btu. This implies that 0.40 million Btu were lost by the water to the ambient environment through the insulation.

Space Cooling - Space cooling was required on all of the working days of the month. The space cooling load was 18.78 million Btu. Water from the chilled water storage was pumped through the air duct heat exchangers to remove 8.06 million Btu from the air. Chilled water from the central plant was required to assist in supporting the cooling load during all but two of the days of the month when space cooling was required. This resulted in a space cooling solar fraction of 43 percent for the month of June.

D. Observations

The most significant anomaly observed during the month of June was the drop in collector efficiency. Normal collector efficiency has averaged near 14 percent, but during May it dropped to 12 percent, and in June it

was 10.1 percent. The loss in efficiency is partially attributable to an increase in cloud cover, which reduces the ratio of direct to total solar radiation. Since these collectors primarily collect direct radiation, this reduces their efficiency.

A collector tracking problem has recently been discovered which also significantly affects collector efficiency. This problem of the collectors mistracking the sun resulted in collection beginning almost an hour later in June than in April, and generally continuing for an hour longer in June than in April. Apparently the mistracking began to occur in May. It should be corrected during July.

Losses from both storage tanks were below their typical levels, which have generally been higher than expected for their design. It is expected that there will always be a significant variance in the calculated values of tank losses. This uncertainty arises from the fact that this calculation involves the measurement of small changes in storage temperature, which may be biased by thermal stratification within the tank, fluctuations in temperatures during the course of the 24-hour period over which it is averaged, and small sensor inaccuracies.

Investigations are being made in an attempt to determine the accuracy of several temperature sensors, and to improve them if possible.

E. Energy Savings

A total electrical energy savings of 0.36 million Btu (107 kwh) was realized. This value assumes that, had there not been a solar energy system, the energy requirements would have been met by an electrical hot water heater and by a conventional electrical heat pump.

III. ACTION STATUS

The accuracy of the several temperature sensors in the space cooling system are being investigated.

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